

Hilti HIT-RE 500-SD mortar with rebar (as anchor)













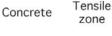


Variable embedm ent

Fire resistanc

SAFEset

Hilti SAFEset technology with hollow drill bit



Seismic ETA-C1

distance and spacing

depth



European Technical Approval



CE conformi ty



Anchor design software

Approvals / certificates

| Description | Authority / Laboratory | No. / date of issue |
|--------------------------------|------------------------|------------------------------|
| European technical approval a) | DIBt, Berlin | ETA-07/0260 / 2013-06-26 |
| ES report icl. seismic | ICC evaluation service | ESR 2322 / 2014-02-01 |
| Fire test report | MFPA, Leipzig | GS-III/B-07-070 / 2008-01-18 |
| Assessment report (fire) | warringtonfire | WF 327804/B / 2013-07-10 |

a) All data given in this section according ETA-07/0260, issue 2013-06-26.

For details see Simplified design method



Basic loading data (for a single anchor)

All data in this section applies to

- Correct setting (See setting instruction)
- No edge distance and spacing influence
- Steel failure
- Base material thickness, as specified in the table
- One typical embedment depth, as specified in the table
- One anchor material, as specified in the tables
- Concrete C 20/25, f_{ck,cube} = 25 N/mm²
- Temperate range I
 - (min. base material temperature: +24°C, max. long term/short term base material temperature: +24°C/40°C)
- Installation temperature range +5°C to +40°C

Embedment depth ^{a)} and base material thickness for the basic loading data. Mean ultimate resistance, characteristic resistance, design resistance, recommended loads.

| | | Data according ETA-07/0260, issue 2013-06-26 | | | | | | | | |
|------------------------------|-----|--|-----|-----|-----|-----|-----|-----|-----|--|
| Anchor size | Ø8 | Ø10 | Ø12 | Ø14 | Ø16 | Ø20 | Ø25 | Ø28 | Ø32 | |
| Typical embedment depth [mm] | 80 | 90 | 110 | 125 | 125 | 170 | 210 | 270 | 300 | |
| Base material thickness [mm] | 110 | 120 | 145 | 165 | 165 | 220 | 275 | 340 | 380 | |

a) The allowed range of embedment depth is shown in the setting details. The corresponding load values can be calculated according to the simplified design method.

Mean ultimate resistance: concrete C 20/25 - f_{ck,cube} = 25 N/mm², anchor rebar BSt 500S

| | | | | Data according ETA-07/0260, issue 2013-06-26 | | | | | | | | |
|---------------------------|-----------|------|------|--|------|------|------|-------|-------|-------|-------|--|
| Anchor size | | | | | Ø12 | Ø14 | Ø16 | Ø20 | Ø25 | Ø28 | Ø32 | |
| Non cracked c | oncrete | | | | | | | | | | | |
| Tensile N _{Ru,m} | BSt 500 S | [kN] | 29,4 | 45,2 | 65,1 | 89,3 | 94,1 | 149,2 | 204,9 | 298,7 | 349,9 | |
| Shear V _{Ru,m} | BSt 500 S | [kN] | 14,7 | 23,1 | 32,6 | 44,1 | 57,8 | 90,3 | 141,8 | 177,5 | 232,1 | |
| Cracked concr | ete | | | | | | | | | | | |
| Tensile N _{Ru,m} | BSt 500 S | [kN] | 23,8 | 33,5 | 46,1 | 57,0 | 65,2 | 110,8 | 146,1 | 228,7 | 268,1 | |
| Shear V _{Ru,m} | BSt 500 S | [kN] | 14,7 | 23,1 | 32,6 | 44,1 | 57,8 | 90,3 | 141,8 | 177,5 | 232,1 | |

Characteristic resistance: concrete C 20/25 - fck.cube = 25 N/mm², anchor rebar BSt 500 S

| | | 10101 | | | - 011,01 | 400 | 0.0000000 | , | | | | | |
|-------------------------|-----------|-------|------|--|----------|------|-----------|-------|-------|-------|-------|--|--|
| | | | | Data according ETA-07/0260, issue 2013-06-26 | | | | | | | | | |
| Anchor size | | | Ø8 | Ø10 | Ø12 | Ø14 | Ø16 | Ø20 | Ø25 | Ø28 | Ø32 | | |
| Non cracked concrete | | | | | | | | | | | | | |
| Tensile N _{Rk} | BSt 500 S | [kN] | 28,0 | 42,4 | 58,3 | 70,6 | 70,6 | 111,9 | 153,7 | 224,0 | 262,4 | | |
| Shear V _{Rk} | BSt 500 S | [kN] | 14,0 | 22,0 | 31,0 | 42,0 | 55,0 | 86,0 | 135,0 | 169,0 | 221,0 | | |
| Cracked cond | rete | | | | | | | | | | | | |
| Tensile N _{Rk} | BSt 500 S | [kN] | 16,1 | 22,6 | 31,1 | 38,5 | 44,0 | 74,8 | 109,6 | 154,4 | 181,0 | | |
| Shear V _{Rk} | BSt 500 S | [kN] | 14,0 | 22,0 | 31,0 | 42,0 | 55,0 | 86,0 | 135,0 | 169,0 | 221,0 | | |

Design resistance: concrete C 20/25 - f_{ck.cube} = 25 N/mm², anchor rebar BSt 500 S

| - | THE PERSON NAMED IN COLUMN | | | | | | | • • | 2012 20 | | | |
|-------------------------|----------------------------|------|------|--|------|------|------|------|---------|-------|-------|--|
| | | | | Data according ETA-07/0260, issue 2013-06-26 | | | | | | | | |
| Anchor size | | | Ø8 | Ø10 | Ø12 | Ø14 | Ø16 | Ø20 | Ø25 | Ø28 | Ø32 | |
| Non cracked concrete | | | | | | | | | | | | |
| Tensile N _{Rd} | BSt 500 S | [kN] | 16,8 | 23,6 | 32,4 | 39,2 | 33,6 | 53,3 | 73,2 | 106,7 | 125,0 | |
| Shear V _{Rd} | BSt 500 S | [kN] | 9,3 | 14,7 | 20,7 | 28,0 | 36,7 | 57,3 | 90,0 | 112,7 | 147,3 | |
| Cracked conc | rete | | | | | | | | | | | |
| Tensile N _{Rd} | BSt 500 S | [kN] | 8,9 | 12,6 | 17,3 | 21,4 | 20,9 | 35,6 | 52,2 | 73,5 | 86,2 | |
| Shear V _{Rd} | BSt 500 S | [kN] | 9,3 | 14,7 | 20,7 | 28,0 | 36,7 | 57,3 | 90,0 | 112,7 | 147,3 | |



Recommended loads a): concrete C 20/25 - f_{ck,cube} = 25 N/mm², anchor rebar BSt 500 S

| | | | | Data according ETA-07/0260, issue 2013-06-26 | | | | | | | | | |
|--------------------------|-----------|------|------|--|------|------|------|------|------|------|-------|--|--|
| Anchor size | | | Ø8 | Ø10 | Ø12 | Ø14 | Ø16 | Ø20 | Ø25 | Ø28 | Ø32 | | |
| Non cracked | concrete | | | | | | | | | | | | |
| Tensile N _{rec} | BSt 500 S | [kN] | 12,0 | 16,8 | 23,1 | 28,0 | 24,0 | 38,1 | 52,3 | 76,2 | 89,3 | | |
| Shear V _{rec} | BSt 500 S | [kN] | 6,7 | 10,5 | 14,8 | 20,0 | 26,2 | 41,0 | 64,3 | 80,5 | 105,2 | | |
| Cracked cond | rete | | | | | | | | | | | | |
| Tensile N _{rec} | BSt 500 S | [kN] | 6,4 | 9,0 | 12,3 | 15,3 | 15,0 | 25,4 | 37,3 | 52,5 | 61,5 | | |
| Shear V _{rec} | BSt 500 S | [kN] | 6,7 | 10,5 | 14,8 | 20,0 | 26,2 | 41,0 | 64,3 | 80,5 | 105,2 | | |

a) With overall partial safety factor for action $\gamma = 1.4$. The partial safety factors for action depend on the type of loading and shall be taken from national regulations.

Service temperature range

Hilti HIT-RE 500-SD injection mortar may be applied in the temperature ranges given below. An elevated base material temperature may lead to a reduction of the design bond resistance.

| Temperature range | Base material temperature | Maximum long term base material temperature | Maximum short term base material temperature |
|-----------------------|---------------------------|---|--|
| Temperature range I | -40 °C to +40 °C | +24 °C | +40 °C |
| Temperature range II | -40 °C to +58 °C | +35 °C | +58 °C |
| Temperature range III | -40 °C to +70 °C | +43 °C | +70 °C |

Max short term base material temperature

Short-term elevated base material temperatures are those that occur over brief intervals, e.g. as a result of diurnal cycling.

Max long term base material temperature

Long-term elevated base material temperatures are roughly constant over significant periods of time.

Materials

Mechanical properties of rebar BSt 500S

| | | | | Dat | ta accor | ding ET/ | 4-07/026 | 0, issue | 2013-06 | -26 | |
|--|-----------|---------|------|------|----------|----------|----------|----------|---------|-------|-------|
| Anchor siz | e | | Ø8 | Ø10 | Ø12 | Ø14 | Ø16 | Ø20 | Ø25 | Ø28 | Ø32 |
| Nominal tensile strength f _{uk} | BSt 500 S | [N/mm²] | 550 | 550 | 550 | 550 | 550 | 550 | 550 | 550 | 550 |
| Yield strength f _{yk} | BSt 500 S | [N/mm²] | 500 | 500 | 500 | 500 | 500 | 500 | 500 | 500 | 500 |
| Stressed cross- section A _s | BSt 500 S | [mm²] | 50,3 | 78,5 | 113,1 | 153,9 | 201,1 | 314,2 | 490,9 | 615,8 | 804,2 |
| Moment of resistance W | BSt 500 S | [mm³] | 50,3 | 98,2 | 169,6 | 269,4 | 402,1 | 785,4 | 1534 | 2155 | 3217 |

Material quality

| Part | Material |
|--------------------|--|
| rebar BSt 500 S | Geometry and mechanical properties according to DIN 488-2:1986 or E DIN 488-2:2006 |

378



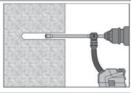
Setting

installation equipment

| Anchor size | Ø8 | Ø10 | Ø12 | Ø14 | Ø16 | Ø20 | Ø25 | Ø28 | Ø32 |
|---------------|---|-----|--------|-----|---------------|-----|-----|-----|--------|
| Rotary hammer | | TE | 2 – TE | 16 | TE 40 – TE 70 | | | | |
| Other tools | compressed air gun or blow out pump, set of cleaning brushes, dispenser | | | | | | | | penser |

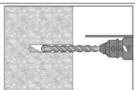
Setting instruction

Bore hole drilling



Drill hole to the required embedment depth with an appropriately sized Hilti TE-CD or TE-YD hollow drill bit with Hilti vacuum attachment. This drilling system removes the dust and cleans the borehole during drilling when using in accordance with the user's manual.

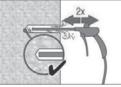
After drilling is complete, proceed to the "injection preparation" step in the instructions for use.



Drill Hole to the required embedment depth with a hammer drill set in rotation-hammer mode using an appropriately sized carbide drill bit.

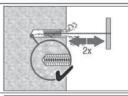
Bore hole cleaning Just before setting an anchor, the bore hole must be free of dust and debris.

Compressed air cleaning (CAC) for all bore hole diameters do and all bore hole depth ho



Blow 2 times from the back of the hole (if needed with nozzle extension) over the hole length with oil-free compressed air (min. 6 bar at 6 m³/h) until return air stream is free of noticeable dust.

Bore hole diameter \geq 32 mm the compressor must supply a minimum air flow of 140 m³/hour.



Brush 2 times with the specified brush size by inserting the steel brush Hilti HIT-RB to the back of the hole (if needed with extension) in a twisting motion and removing it.

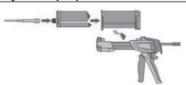
The brush must produce natural resistance as it enters the bore hole -- if not the brush is too small and must be replaced with the proper brush diameter.



Blow again with compressed air 2 times until return air stream is free of noticeable dust.



Injection preparation



Tightly attach new Hilti mixing nozzle HIT-RE-M to foil pack manifold (snug fit). Do not modify the mixing nozzle.

Observe the instruction for use of the dispenser and the mortar. Check foil pack holder for proper function. Do not use damaged foil packs / holders. Insert foil pack into foil pack holder and put holder into HIT-dispenser.

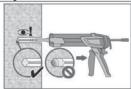


The foil pack opens automatically as dispensing is initiated. Discard initial adhesive. Depending on the size of the foil pack an initial amount of adhesive has to be discarded.

Discard quantities are:

- 3 strokes for 330 ml foil pack,
- 4 strokes for 500 ml foil pack,
- 65 ml for 1400 ml foil pack ≤ 5°C.

Inject adhesive from the back of the borehole without forming air voids

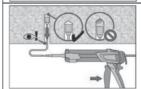


Inject the adhesive starting at the back of the hole, slowly withdrawing the mixer with each trigger pull.

Fill holes approximately 2/3 full It is required that the annular gap between the anchor and the concrete is completely filled with adhesive along the embedment length.



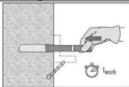
After injection is completed, depressurize the dispenser by pressing the release trigger. This will prevent further adhesive discharge from the mixer.



Overhead installation and/or installation with embedment depth hef > 250mm

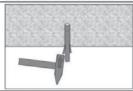
For overhead installation the injection is only possible with the aid of extensions and piston plugs. Assemble HIT-RE-M mixer, extension(s) and appropriately sized piston plug (HIT-SZ). Insert piston plug to back of the hole and inject adhesive. During injection the piston plug will be naturally extruded out of the bore hole by the adhesive pressure.

Setting the element

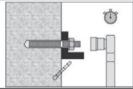


Before use, verify that the element is dry and free of oil and other contaminants.

Mark and set element to the required embedment depth untill working time t_{work} has elapsed.



For overhead installation use piston plugs and fix embedded parts with e.g. wedges HIT-OHW.



Loading the anchor:

After required curing time toure the anchor can be loaded.

The applied installation torque shall not exceed given Tmax.

For detailed information on installation see instruction for use given with the package of the product



Curing time for general conditions

| Da | Data according ETA-07/0260, issue 2013-06-26 | | | | | | | | | | |
|----------------------------------|--|---|--|--|--|--|--|--|--|--|--|
| Temperature of the base material | Working time in which anchor can be inserted and adjusted t _{gel} | Curing time before anchor can be fully loaded t _{cure} | | | | | | | | | |
| 40 °C | 12 min | 4 h | | | | | | | | | |
| 30 °C to 39 °C | 12 min | 8 h | | | | | | | | | |
| 20 °C to 29 °C | 20 min | 12 h | | | | | | | | | |
| 15 °C to 19 °C | 30 min | 24 h | | | | | | | | | |
| 10 °C to 14 °C | 90 min | 48 h | | | | | | | | | |
| 5 °C to 9 °C | 120 min | 72 h | | | | | | | | | |

Setting details

| | | | | $\begin{array}{c ccccccccccccccccccccccccccccccccccc$ | | | | | | | | |
|---|----------------------------|------|---|---|---|-----|----------------------|-----------------------|---------------------|----------------------|--------------------|--|
| Anchor size | | | Ø8 | Ø10 | Ø12 | Ø14 | Ø16 | Ø20 | Ø25 | Ø28 | Ø32 | |
| Nominal diameter of drill bit | d ₀ | [mm] | 12 | 14 | 16 | 18 | 20 | 25 | 32 | 35 | 40 | |
| Effective anchorage | h _{ef,min} | [mm] | 60 | 60 | 70 | 75 | 80 | 90 | 100 | 112 | 128 | |
| and drill hole depth range a) | $h_{\text{ef},\text{max}}$ | [mm] | 160 | 200 | 240 | 280 | 320 | 400 | 500 | 560 | 640 | |
| Minimum base material thickness | h _{min} | [mm] | | | | | | h _{ef} + 2 d | 0 | | | |
| Minimum spacing | S _{min} | [mm] | 40 | 50 | 60 | 70 | 80 | 100 | 125 | 140 | 160 | |
| Minimum edge distance | C _{min} | [mm] | 40 | 50 | 60 | 70 | 80 | 100 | 125 | 140 | 160 | |
| Critical spacing for splitting failure | S _{cr,sp} | | | | | | 2 c _{cr,sp} | | | | | |
| Critical edge distance for splitting failure b) | C _{cr,sp} | [mm] | 1,0 · n_{ef} for $n / n_{ef} \ge 2,0$ 4,6 n_{ef} - 1,8 n_{ef} for 2,0 > n_{ef} > 1,3 | | | | | | | | | |
| | | | 2,26 h _{ef} | | for n / n _{ef} ≤ 1,3 | | | , | 1,0·h _{ef} | 2,26·h _{ef} | C _{cr,sp} | |
| Critical spacing for concrete cone failure | S _{cr,N} | | | | | | $2 c_{cr,N}$ | | | | | |
| Critical edge distance for concrete cone failure c) | C _{cr,N} | | | | | | 1,5 h _{ef} | | | | | |
| | | | h | | \$ | |) | | | | | |

For spacing (edge distance) smaller than critical spacing (critical edge distance) the design loads have to be reduced.

- a) $h_{ef,min} \le h_{ef} \le h_{ef,max}$ (h_{ef} : embedment depth)
- b) h: base material thickness (h ≥ h_{min})
- c) The critical edge distance for concrete cone failure depends on the embedment depth h_{ef} and the design bond resistance. The simplified formula given in this table is on the save side.



Simplified design method

Simplified version of the design method according ETAG 001, TR 029. Design resistance according data given in ETA-07/0260, issue 2009-01-12.

- Influence of concrete strength
- Influence of edge distance
- Influence of spacing
- Valid for a group of two anchors. (The method may also be applied for anchor groups with more than two anchors or more than one edge distance. The influencing factors must then be considered for each edge distance and spacing. The calculated design loads are then on the save side: They will be lower than the exact values according ETAG 001, TR 029. To avoid this, it is recommended to use the anchor design software PROFIS anchor)

The design method is based on the following simplification:

No different loads are acting on individual anchors (no eccentricity)

The values are valid for one anchor.

For more complex fastening applications please use the anchor design software PROFIS Anchor.

Tension loading

The design tensile resistance is the lower value of

- Steel resistance: N_R

- Combined pull-out and concrete cone resistance:

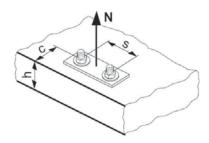
$$N_{Rd,p} = N^0_{Rd,p} \cdot f_{B,p} \cdot f_{1,N} \cdot f_{2,N} \cdot f_{3,N} \cdot f_{h,p} \cdot f_{re,N}$$

- Concrete cone resistance: $N_{Rd,c} = N_{Rd,c}^0 \cdot f_B \cdot f_{1,N} \cdot f_{2,N} \cdot f_{3,N} \cdot f_{h,N} \cdot f_{re,N}$

Concrete splitting resistance (only non-cracked concrete):

$$N_{Rd,sp} = N_{Rd,c}^0 \cdot f_B \cdot f_{1,sp} \cdot f_{2,sp} \cdot f_{3,sp} \cdot f_{h,N} \cdot$$

 $f_{re,N}$



Basic design tensile resistance

Design steel resistance N_{Rd.s}

| | | | | Data according ETA-07/0260, issue 2013-06-26 | | | | | | | | | |
|------------|-----------|------|------|--|------|------|------|-------|-------|-------|-------|--|--|
| Ancho | or size | | Ø8 | Ø10 | Ø12 | Ø14 | Ø16 | Ø20 | Ø25 | Ø28 | Ø32 | | |
| $N_{Rd,s}$ | BSt 500 S | [kN] | 20,0 | 30,7 | 44,3 | 60,7 | 79,3 | 123,6 | 192,9 | 242,1 | 315,7 | | |



Design combined pull-out and concrete cone resistance

 $N_{Rd,p} = N^0_{Rd,p} \cdot f_{B,p} \cdot f_{1,N} \cdot f_{2,N} \cdot f_{3,N} \cdot f_{h,p} \cdot f_{re,N}$

| | | | | Dat | a accor | ding ETA | A-07/026 | 0, issue | 2013-06 | -26 | |
|---------------------------------|----------------------------|------|------|------|---------|----------|----------|----------|---------|-------|-------|
| Ancho | or size | | Ø8 | Ø10 | Ø12 | Ø14 | Ø16 | Ø20 | Ø25 | Ø28 | Ø32 |
| Typica h _{ef,typ} [| al embedment depth [mm] | | 80 | 90 | 110 | 125 | 125 | 170 | 210 | 270 | 300 |
| Non cr | acked concrete | | | | | | | | | | |
| N ⁰ _{Rd,p} | Temperature range I | [kN] | 16,8 | 23,6 | 34,6 | 42,8 | 41,9 | 71,2 | 102,1 | 147,0 | 186,7 |
| N ⁰ _{Rd,p} | Temperature range II | [kN] | 13,4 | 18,8 | 27,6 | 36,7 | 32,9 | 56,0 | 86,4 | 113,1 | 143,6 |
| N ⁰ _{Rd,p} | Temperature range III | [kN] | 7,8 | 11,0 | 16,1 | 21,4 | 20,9 | 33,1 | 51,1 | 67,9 | 86,2 |
| Cracke | ed concrete | | | | | | | | | | |
| N ⁰ _{Rd,p} | Temperature range I | [kN] | 8,9 | 12,6 | 17,3 | 21,4 | 20,9 | 35,6 | 55,0 | 73,5 | 86,2 |
| N ⁰ _{Rd,p} | Temperature range II | [kN] | 7,3 | 10,2 | 13,8 | 18,3 | 18,0 | 28,0 | 43,2 | 56,5 | 71,8 |
| N ⁰ _{Rd,p} | Temperature range III | [kN] | 4,5 | 5,5 | 8,1 | 10,7 | 10,5 | 15,3 | 23,6 | 33,9 | 43,1 |

Design concrete cone resistance $N_{Rd,c} = N^0_{Rd,c} \cdot f_B \cdot f_{1,N} \cdot f_{2,N} \cdot f_{3,N} \cdot f_{h,N} \cdot f_{re,N}$ Design splitting resistance a) $N_{Rd,sp} = N^0_{Rd,c} \cdot f_B \cdot f_{1,sp} \cdot f_{2,sp} \cdot f_{3,sp} \cdot f_{h,N} \cdot f_{re,N}$

| | | | | Data according ETA-07/0260, issue 2013-06-26 | | | | | | | | | |
|--------------------------------|----------------------|------|------|--|------|------|------|------|------|-------|-------|--|--|
| Ancho | or size | | Ø8 | Ø10 | Ø12 | Ø14 | Ø16 | Ø20 | Ø25 | Ø28 | Ø32 | | |
| N ⁰ _{Rd,c} | Non cracked concrete | [kN] | 20,1 | 24,0 | 32,4 | 39,2 | 33,6 | 53,3 | 73,2 | 106,7 | 125,0 | | |
| N ⁰ _{Rd,c} | Cracked concrete | [kN] | 14,3 | 17,1 | 23,1 | 28,0 | 24,0 | 38,0 | 52,2 | 76,1 | 89,1 | | |

a) Splitting resistance must only be considered for non-cracked concrete

Influencing factors

Influence of concrete strength on combined pull-out and concrete cone resistance

| Concrete strength designation (ENV 206) | C 20/25 | C 25/30 | C 30/37 | C 35/45 | C 40/50 | C 45/55 | C 50/60 |
|--|---------|---------|---------|---------|---------|---------|---------|
| $f_{B,p} = (f_{ck,cube}/25N/mm^2)^{0.1}$ | 1 | 1,02 | 1,04 | 1,06 | 1,07 | 1,08 | 1,09 |

a) f_{ck,cube} = concrete compressive strength, measured on cubes with 150 mm side length

Influence of embedment depth on combined pull-out and concrete cone resistance

$$f_{h,p} = h_{ef}/h_{ef,typ}$$

Influence of concrete strength on concrete cone resistance

| Concrete strength designati (ENV 206) | on C 20/25 | C 25/30 | C 30/37 | C 35/45 | C 40/50 | C 45/55 | C 50/60 |
|---------------------------------------|------------|---------|---------|---------|---------|---------|---------|
| $f_B = (f_{ck,cube}/25N/mm^2)^{1/2}$ | 1 | 1,1 | 1,22 | 1,34 | 1,41 | 1,48 | 1,55 |

a) f_{ck,cube} = concrete compressive strength, measured on cubes with 150 mm side length



Influence of edge distance a)

| C/C _{cr,N} | 0,1 | 0,2 | 0,3 | 0,4 | 0,5 | 0,6 | 0,7 | 0,8 | 0,9 | 1 |
|--|------|------|------|------|------|------|------|------|------|----|
| c/c _{cr,sp} | | | | | | | | | | |
| $f_{1,N} = 0,7 + 0,3 \cdot c/c_{cr,N}$ | 0.73 | 0.76 | 0.79 | 0.82 | 0,85 | 0,88 | 0,91 | 0.94 | 0.97 | 1 |
| $f_{1,sp} = 0.7 + 0.3 \cdot c/c_{cr,sp}$ | 0,73 | 0,70 | 0,79 | 0,02 | 0,05 | 0,00 | 0,91 | 0,34 | 0,97 | , |
| | | | | | | | | | | |
| $f_{2,N} = 0.5 \cdot (1 + c/c_{cr,N})$ | 0.55 | 0.60 | 0.05 | 0.70 | 0.75 | 0.00 | 0.05 | 0.00 | 0.05 | 4 |
| $f_{2,sp} = 0.5 \cdot (1 + c/c_{cr,sp})$ | 0,55 | 0,60 | 0,65 | 0,70 | 0,75 | 0,80 | 0,85 | 0,90 | 0,95 | -1 |

a) The the edge distance shall not be smaller than the minimum edge distance c_{min} given in the table with the setting details. These influencing factors must be considered for every edge distance smaller than the critical edge distance.

Influence of anchor spacing a)

| s/s _{cr,N} | 0,1 | 0,2 | 0,3 | 0,4 | 0,5 | 0,6 | 0,7 | 0,8 | 0,9 | 1 |
|--|------|------|------|------|------|------|------|------|------|---|
| $f_{3,N} = 0,5\cdot(1 + s/s_{cr,N})$ | 0,55 | 0,60 | 0,65 | 0.70 | 0,75 | 0,80 | 0,85 | 0,90 | 0,95 | 1 |
| $f_{3,sp} = 0.5 \cdot (1 + s/s_{cr,sp})$ | 0,55 | 0,00 | 0,00 | 0,70 | 0,75 | 0,00 | 0,00 | 0,30 | 0,95 | |

a) The anchor spacing shall not be smaller than the minimum anchor spacing s_{min} given in the table with the setting details. This influencing factor must be considered for every anchor spacing.

Influence of embedment depth on concrete cone resistance

$$f_{h,N} = (h_{ef}/h_{ef,typ})^{1,5}$$

Influence of reinforcement

| h _{ef} [mm] | 40 | 50 | 60 | 70 | 80 | 90 | ≥ 100 |
|---|--------|---------|-------------------|---------|--------|---------|-------|
| $f_{re,N} = 0.5 + h_{ef}/200 \text{mm} \le 1$ | 0,7 a) | 0,75 a) | 0,8 ^{a)} | 0,85 a) | 0,9 a) | 0,95 a) | 1 |

a) This factor applies only for dense reinforcement. If in the area of anchorage there is reinforcement with a spacing ≥ 150 mm (any diameter) or with a diameter ≤ 10 mm and a spacing ≥ 100 mm, then a factor f_{re} = 1 may be applied.

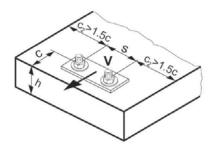
Shear loading

The design shear resistance is the lower value of

Steel resistance: V_{Rd,s}

Concrete pryout resistance: $V_{Rd,cp} = k \cdot \text{lower value of } N_{Rd,p} \text{ and } N_{Rd,c}$

- Concrete edge resistance: $V_{Rd,c} = V_{Rd,c}^0 \cdot f_B \cdot f_b \cdot f_4 \cdot f_{hef} \cdot f_c$





Basic design shear resistance

Design steel resistance V_{Rd,s}

| | | | Data according ETA-07/0260, issue 2013-06-26 | | | | | | | | | | |
|------------|-----------|------|--|------|------|------|------|------|------|-------|-------|--|--|
| Ancho | or size | | Ø8 | Ø10 | Ø12 | Ø14 | Ø16 | Ø20 | Ø25 | Ø28 | Ø32 | | |
| $V_{Rd,s}$ | BSt 500 S | [kN] | 9,3 | 14,7 | 20,7 | 28,0 | 36,7 | 57,3 | 90,0 | 112,7 | 147,3 | | |

Design concrete pryout resistance $V_{Rd,cp}$ = lower value^{a)} of $k \cdot N_{Rd,p}$ and $k \cdot N_{Rd,c}$

 $k = 1 \text{ for } h_{ef} < 60 \text{ mm}$ $k = 2 \text{ for } h_{ef} \ge 60 \text{ mm}$

a) N_{Rd,p}: Design combined pull-out and concrete cone resistance

N_{Rd,c}: Design concrete cone resistance

Design concrete edge resistance $V_{Rd,c} = V^0_{Rd,c} \cdot f_B \cdot f_b \cdot f_h \cdot f_4 \cdot f_{hef} \cdot f_c$

| | | Data according ETA-07/0260, issue 2013-06-26 | | | | | | | | | | | |
|--------------------------------|------|--|-----|------|------|------|------|---------|-----------|------|--|--|--|
| Anchor size | | Ø8 | Ø10 | Ø12 | Ø14 | Ø16 | Ø20 | Ø25 | Ø28 | Ø32 | | | |
| Non-cracked concrete | | | | | | | | | | | | | |
| V ⁰ _{Rd,c} | [kN] | 5,9 | 8,6 | 11,6 | 15,0 | 18,7 | 27,0 | 39,2 | 47,3 | 59,0 | | | |
| Cracked concrete | | | - | ,,,, | | | | 72 72 7 | 22 101 00 | | | | |
| V ⁰ _{Rd,c} | [kN] | 4,2 | 6,1 | 8,2 | 10,6 | 13,2 | 19,2 | 27,7 | 33,5 | 41,8 | | | |

Influencing factors

Influence of concrete strength

| Concrete strength designation (ENV 206) | C 20/25 | C 25/30 | C 30/37 | C 35/45 | C 40/50 | C 45/55 | C 50/60 |
|---|---------|---------|---------|---------|---------|---------|---------|
| $f_B = (f_{ck,cube}/25N/mm^2)^{1/2 \ a)}$ | 1 | 1,1 | 1,22 | 1,34 | 1,41 | 1,48 | 1,55 |

a) f_{ck,cube} = concrete compressive strength, measured on cubes with 150 mm side length

Influence of angle between load applied and the direction perpendicular to the free edge

| Angle ß | 0° | 10° | 20° | 30° | 40° | 50° | 60° | 70° | 80° | ≥ 90° |
|---|----|------|------|------|------|------|------|------|------|-------|
| $f_{\beta} = \sqrt{\frac{1}{(\cos \alpha_{V})^{2} + \left(\frac{\sin \alpha_{V}}{2,5}\right)^{2}}}$ | 1 | 1,01 | 1,05 | 1,13 | 1,24 | 1,40 | 1,64 | 1,97 | 2,32 | 2,50 |

Influence of base material thickness

| h/c | 0,15 | 0,3 | 0,45 | 0,6 | 0,75 | 0,9 | 1,05 | 1,2 | 1,35 | ≥ 1,5 |
|---|------|------|------|------|------|------|------|------|------|-------|
| $f_h = \{h/(1,5 \cdot c)\}^{1/2} \le 1$ | 0,32 | 0,45 | 0,55 | 0,63 | 0,71 | 0,77 | 0,84 | 0,89 | 0,95 | 1,00 |



Influence of anchor spacing and edge distance ^{a)} for concrete edge resistance: $f_4 = (c/h_{ef})^{1,5} \cdot (1 + s / [3 \cdot c]) \cdot 0,5$

| | | | _ | | • | | | | 101.70.000 | | | | | | | |
|-------------------|--------|------|------|------|------|------|------|---------|------------|-------|-------------------|------|------|------|-----------|------|
| | Single | | | | | | Grou | up of t | wo an | chors | s/h _{ef} | | | | | |
| c/h _{ef} | anchor | 0,75 | 1,50 | 2,25 | 3,00 | 3,75 | 4,50 | 5,25 | 6,00 | 6,75 | 7,50 | 8,25 | 9,00 | 9,75 | 10, 50 | 11, |
| 0.50 | 0,35 | 0,27 | 0,35 | 0,35 | 0,35 | 0,35 | 0,35 | 0,35 | 0,35 | 0,35 | 0,35 | 0,35 | 0,35 | 0,35 | 0,35 | 0,35 |
| 0,50 | | | | | | | | _ | | | | | | | | |
| 0,75 | 0,65 | 0,43 | 0,54 | 0,65 | 0,65 | 0,65 | 0,65 | 0,65 | 0,65 | 0,65 | 0,65 | 0,65 | 0,65 | 0,65 | 0,65 | 0,65 |
| 1,00 | 1,00 | 0,63 | 0,75 | 0,88 | 1,00 | 1,00 | 1,00 | 1,00 | 1,00 | 1,00 | 1,00 | 1,00 | 1,00 | 1,00 | 1,00 | 1,00 |
| 1,25 | 1,40 | 0,84 | 0,98 | 1,12 | 1,26 | 1,40 | 1,40 | 1,40 | 1,40 | 1,40 | 1,40 | 1,40 | 1,40 | 1,40 | 1,40 | 1,40 |
| 1,50 | 1,84 | 1,07 | 1,22 | 1,38 | 1,53 | 1,68 | 1,84 | 1,84 | 1,84 | 1,84 | 1,84 | 1,84 | 1,84 | 1,84 | 1,84 | 1,84 |
| 1,75 | 2,32 | 1,32 | 1,49 | 1,65 | 1,82 | 1,98 | 2,15 | 2,32 | 2,32 | 2,32 | 2,32 | 2,32 | 2,32 | 2,32 | 2,32 | 2,32 |
| 2,00 | 2,83 | 1,59 | 1,77 | 1,94 | 2,12 | 2,30 | 2,47 | 2,65 | 2,83 | 2,83 | 2,83 | 2,83 | 2,83 | 2,83 | 2,83 | 2,83 |
| 2,25 | 3,38 | 1,88 | 2,06 | 2,25 | 2,44 | 2,63 | 2,81 | 3,00 | 3,19 | 3,38 | 3,38 | 3,38 | 3,38 | 3,38 | 3,38 | 3,38 |
| 2,50 | 3,95 | 2,17 | 2,37 | 2,57 | 2,77 | 2,96 | 3,16 | 3,36 | 3,56 | 3,76 | 3,95 | 3,95 | 3,95 | 3,95 | 3,95 | 3,95 |
| 2,75 | 4,56 | 2,49 | 2,69 | 2,90 | 3,11 | 3,32 | 3,52 | 3,73 | 3,94 | 4,15 | 4,35 | 4,56 | 4,56 | 4,56 | 4,56 | 4,56 |
| 3,00 | 5,20 | 2,81 | 3,03 | 3,25 | 3,46 | 3,68 | 3,90 | 4,11 | 4,33 | 4,55 | 4,76 | 4,98 | 5,20 | 5,20 | 5,20 | 5,20 |
| 3,25 | 5,86 | 3,15 | 3,38 | 3,61 | 3,83 | 4,06 | 4,28 | 4,51 | 4,73 | 4,96 | 5,18 | 5,41 | 5,63 | 5,86 | 5,86 | 5,86 |
| 3,50 | 6,55 | 3,51 | 3,74 | 3,98 | 4,21 | 4,44 | 4,68 | 4,91 | 5,14 | 5,38 | 5,61 | 5,85 | 6,08 | 6,31 | 6,55 | 6,55 |
| 3,75 | 7,26 | 3,87 | 4,12 | 4,36 | 4,60 | 4.84 | 5,08 | 5,33 | 5,57 | 5,81 | 6,05 | 6,29 | 6,54 | 6,78 | 7,02 | 7,26 |
| 4,00 | 8,00 | 4,25 | 4,50 | 4,75 | 5.00 | 5.25 | 5,50 | 5.75 | 6,00 | 6,25 | 6,50 | 6.75 | 7,00 | 7,25 | 7,50 | 7,75 |
| 4,25 | 8,76 | 4,64 | 4,90 | 5,15 | 5,41 | 5.67 | 5,93 | 6,18 | 6,44 | 6,70 | 6.96 | 7,22 | 7,47 | 7,73 | 7,99 | 8,25 |
| 4,50 | 9,55 | 5,04 | 5,30 | 5,57 | 5,83 | 6,10 | 6,36 | 6,63 | 6,89 | 7,16 | 7,42 | 7,69 | 7,95 | 8,22 | 8,49 | 8,75 |
| 4,75 | 10,35 | 5,45 | 5,72 | 5,99 | 6,27 | 6,54 | 6,81 | 7,08 | 7,36 | 7,63 | 7,90 | 8,17 | 8,45 | 8,72 | 8,99 | 9,26 |
| 5,00 | 11,18 | 5,87 | 6,15 | 6,43 | 6,71 | 6,99 | 7,27 | 7,55 | 7,83 | 8,11 | 8,39 | 8,66 | 8,94 | 9,22 | 9,50 | 9,78 |
| | | | | | | | | - | | | | | | | 10, | 10, |
| 5,25 | 12,03 | 6,30 | 6,59 | 6,87 | 7,16 | 7,45 | 7,73 | 8,02 | 8,31 | 8,59 | 8,88 | 9,17 | 9,45 | 9,74 | 02 | 31 |
| 5,50 | 12,90 | | | | | | | | | | | | | 10, | 10, | 10, |
| 3,30 | 12,90 | 6,74 | 7,04 | 7,33 | 7,62 | 7,92 | 8,21 | 8,50 | 8,79 | 9,09 | 9,38 | 9,67 | 9,97 | 26 | 55 | 85 |

a) The anchor spacing and the edge distance shall not be smaller than the minimum anchor spacing s_{min} and the minimum edge distance c_{min} .

Influence of embedment depth

| h _{ef} /d | 4 | 4,5 | 5 | 6 | 7 | 8 | 9 | 10 | 11 |
|--|------|------|------|------|------|------|------|------|------|
| $f_{hef} = 0.05 \cdot (h_{ef} / d)^{1.68}$ | 0,51 | 0,63 | 0,75 | 1,01 | 1,31 | 1,64 | 2,00 | 2,39 | 2,81 |
| h _{ef} /d | 12 | 13 | 14 | 15 | 16 | 17 | 18 | 19 | 20 |
| $f_{hef} = 0.05 \cdot (h_{ef} / d)^{1.68}$ | 3,25 | 3,72 | 4,21 | 4,73 | 5,27 | 5,84 | 6,42 | 7,04 | 7,67 |

Influence of edge distance a)

| c/d | 4 | 6 | 8 | 10 | 15 | 20 | 30 | 40 |
|------------------------|------|------|------|------|------|------|------|------|
| $f_c = (d / c)^{0.19}$ | 0,77 | 0,71 | 0,67 | 0,65 | 0,60 | 0,57 | 0,52 | 0,50 |

a) The edge distance shall not be smaller than the minimum edge distance c_{min}.

Combined tension and shear loading

For combined tension and shear loading see section "Anchor Design".



Seismic design C1

Basic loading data for concrete C20/25 - C50/60

All data in this section applies to:

Seismic design according to TR045

The following technical data are based on: ETA-07/0260, issue 2013-06-26

Anchorage depth range

| Anchor size | | | Ф8 | Ф10 | Ф12 | Ф14 | Ф16 | Ф20 | Ф25 | Ф26 | Ф28 | Ф30 | Ф32 |
|---------------------|---------------------|------|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|
| Effective anchorage | h _{ef,min} | [mm] | 60 | 60 | 70 | 80 | 80 | 90 | 100 | 104 | 115 | 120 | 130 |
| depth range | h _{ef,max} | [mm] | 160 | 200 | 240 | 280 | 320 | 400 | 500 | 520 | 540 | 600 | 660 |

Tension resistance in case of seismic performance category C1

| Anchor size | | | Φ8 | Ф10 | Ф12 | Ф14 | Ф16 | Ф20 | Ф25 | Ф26 | Ф28 | Ф30 | Ф32 |
|--|-------------------------|------------|---------|--------|-------|---------|-------|-----|-----|-----|-----|-----|-----|
| Characteristic tensi | on resista | nce to ste | el fail | ure | | | | | | | | | |
| Rebar B500B Acc. to DIN 488:2009 | seis [kN] | 28 | 43 | 62 | 85 | 111 | 173 | 270 | - | 339 | | 442 | |
| Partial safety factor Acc. to DIN 488:2009 | eis [-] | | | ile. | 1,4 | ٠ | R 0 | Öi. | - | 1,4 | - | 1,4 | |
| Characteristic bond | resistanc | e in crack | ed co | ncrete | C20/2 | 5 to C5 | 50/60 | | | | | | |
| Temp. range I: 40°C/24°C | $	au_{Rk,seis}$ | [N/mm²] | 6,4 | 6,4 | 6 | 5,4 | 5,3 | 5 | 4,6 | 4,5 | 4 | 3,6 | 3,4 |
| Temp. range II: 58°C/35°C | $\tau_{\text{Rk,seis}}$ | [N/mm²] | 5,2 | 5,2 | 4,8 | 4,7 | 4,5 | 3,9 | 3,6 | 3,5 | 3,1 | 3,0 | 2,9 |
| Temp. range III: 70°C/43°C | $\tau_{\text{Rk,seis}}$ | [N/mm²] | 3,2 | 2,8 | 2,8 | 2,7 | 2,6 | 2,1 | 2 | 1,9 | 1,8 | 1,8 | 1,7 |
| Partial safety factor | γMp,seis | [-] | | 1 | ,8 | | | | | 2,1 | | | |
| Concrete cone resis | stance and | splitting | resist | ance | | | | | | | | | |
| Partial safety factor γ _{Mc,seis} = [-] | | | 1,8 | | | | 2,1 | | | | | | |

Displacement under tension load in case of seismic performance category C1 1)

| Anchor size | | | Ф8 | Ф10 | Ф12 | Ф14 | Ф16 | Ф20 | Ф25 | Ф26 | Ф28 | Ф30 | Ф32 |
|-----------------|-------------------|------|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|
| Displacement 1) | $\delta_{N,seis}$ | [mm] | 1,5 | 1,7 | 1,9 | 2,1 | 2,3 | 2,7 | 3,2 | 3,3 | 3,5 | 3,7 | 3,9 |

¹⁾ Maximum displacement during cycling (seismic event).

= YMc,seis

Shear resistance in case of seismic performance category C1

| Anchor size | anchor size | | | | Ф12 | Ф14 | Ф16 | Ф20 | Ф25 | Ф26 | Ф28 | Ф30 | Ф32 |
|--|-----------------|-------|--------|---------|--------|-----|-----|-----|-----|-----|-----|-----|-----|
| Characteristic shear resistance to steel failure | | | | | | | | | | | | | |
| Rebar B500B Acc. to DIN 488:2009- 08 | $N_{Rk,s,seis}$ | [kN] | 10 | 15 | 22 | 29 | 39 | 60 | 95 | - | 118 | - | 155 |
| Partial safety factor Acc. to DIN 488:2009- 08 | γMs,seis | [-] | | | | 1,5 | | | | - | 1,5 | - | 1,5 |
| Concrete pryout resis | stance and | concr | ete ed | ge resi | stance | , | | | | 20 | | 71 | |
| Partial safety factor | YMcp,seis | [-] | | | | | | 1,5 | | | | | |



Displacement under shear load in case of seismic performance category C1 1)

| Anchor size | | | Φ8 | Ф10 | Ф12 | Ф14 | Ф16 | Ф20 | Ф25 | Ф26 | Ф28 | Ф30 | Ф32 |
|----------------------------|-------------------|------|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|
| Displacement ¹⁾ | $\delta_{V,seis}$ | [mm] | 3,2 | 3,5 | 3,8 | 4,1 | 4,4 | 5,0 | 5,8 | 5,9 | 6,2 | 6,5 | 6,8 |

¹⁾ Maximum displacement during cycling (seismic event).

For seismic resistent fastening applications please use the anchor design software PROFIS Anchor.